

APPENDIX L

MODULAR HYBRID PIER PRELIMINARY CONSTRUCTION COSTS

Attached on the following pages is a cost estimate based on the current preliminary design of the Modular Hybrid Pier. The costs are presented for a baseline case, a low range case and a high range case. The low range is about 83 percent of the baseline cost and the high range is about 120 percent of the baseline cost.

In most cases any assumptions made in the estimates are given in the background material supporting the estimate. Outside estimators were involved in providing some of the cost estimates.

Concrete Technology Corporation estimated the floating modules FOB their yard in Tacoma, WA. Their estimate is the high range cost given for the Structural Concrete Module Costs. Concrete Technology Corporation has a graving dock and has experience of having constructed a number of projects of similar scale to the MHP.

Manson Construction provided estimates for module to module joining and for the construction of the on-site mooring structures. Their estimates are the high range costs for both the Module to Module Joining and the MHP Mooring Costs. Manson was the general contractor for the floating portion of the Ford Island bridge.

Ed Blessing, and marine cost estimating consultant, also estimated the mooring construction cost. His estimate is the low range cost for the MHP Mooring Cost.

Vasant and Gusler provided the mechanical and electrical utility estimates. They have significant cost estimating experience from the design of utilities for many Navy piers.

It should be noted that all of these cost estimates are based on concept level designs and that the material quantities involved are preliminary estimates.

When comparing costs with recent Navy pier construction it is important to adjust the costs for location, as construction cost factors differ significantly across the United States. A listing of Location Construction Cost Factors from Means 2000 is provided on the following page.

Location Construction Cost Factors from Means 2000			
City	Cost factor	Construction cost vs Norfolk	Construction cost vs San Diego
San Diego	106.6	129.2%	100.0%
Norfolk	82.5	100.0%	77.4%
San Francisco	123.8	150.1%	116.1%
Anchorage	125.2	151.8%	117.4%
Los Angeles	109.6	132.8%	102.8%
Jacksonville	83.6	101.3%	78.4%
Savannah	82.3	99.8%	77.2%
Honolulu	122.3	148.2%	114.7%
Shreveport	80.9	98.1%	75.9%
Boston	116.6	141.3%	109.4%
New York	133.8	162.2%	125.5%
Charleston	94.3	114.3%	88.5%
Seattle	105.0	127.3%	98.5%

Concept Design Cost Estimate- MHP Berthing Facility
 (all costs are installed costs - Navy construction - 2001 \$)

Item	Units	Low Range Cost	Baseline Cost	High Range Cost	Comments
Costs are for a 1300 ft MHP berthing facility with 2 mooring elements.					
Structural Concrete Module Costs		\$14,604,800	\$18,256,000	\$21,580,648	
Corrosion Resistant Reinforcing		\$1,800,000	\$2,960,000	\$4,440,000	material cost only - labor incl in module costs
Ancillary items		\$2,934,400	\$2,934,400	\$2,934,400	See attached listing
Module to Module Joining Cost		\$750,000	\$1,089,000	\$1,404,000	
MHP Mooring Cost		\$1,844,400	\$2,004,896	\$3,970,000	2 moorings
MHP Operations Deck Ramp Cost		\$385,209	\$428,010	\$470,811	98 ft long ramp steel construciton
MHP Service Deck Ramp Cost		\$245,879	\$258,820	\$284,702	98 ft long ramp steel construction
MHP Electrical Utilities		\$7,023,830	\$7,804,255	\$8,194,468	
MHP Mechanical Utilities		\$2,192,366	\$2,435,962	\$2,557,760	
Assumed 500 mile tow for module delivery		\$318,240	\$374,400	\$411,840	
Subtotal		\$32,099,123	\$38,545,743	\$46,248,629	
10% for miscellaneous undesignated details		\$3,209,912	\$3,854,574	\$4,624,863	
Total concept level construction cost estimate		\$35,309,036	\$42,400,317	\$50,873,492	

Structural Concrete Module Cost - MHP Berthing Facility - Baseline Cost					
(all costs are installed costs - Navy construction - 2001 \$)					
Item	Units	Unit price	Quantity	Total	Comments
Graving dock rental				\$1,000,000	Assumption
Module CIP keel slab	CY	\$450	940	\$423,000	
Service deck including crossover	CY	\$550	770	\$423,500	
Service deck (auxiliary support area)	SF				Auxillary space not included
Operations deck	CY	\$400	1790	\$716,000	
Exterior longitudinal walls	CY	\$1,000	610	\$610,000	
Interior longitudinal walls	CY	\$950	730	\$693,500	
Interior transverse walls	CY	\$1,000	310	\$310,000	
End walls	CY	\$1,100	210	\$231,000	
Concrete stairs	CY	\$800	50	\$40,000	
Concrete in mooring area	CY	\$900	130	\$117,000	
Cost of bare concrete module				\$4,564,000	
			Total quantity	5540	
Average \$/yard of concrete		\$823.83			
Average \$/SF of operations deck		\$159.58			
Average \$/SF for operations deck + service deck		\$104.80			
Total for 4 modules				\$18,256,000	Includes reinforcing and prestress
Module to module joining, mooring, and utilities are in addition to this bare concrete cost.					

August 10, 2001

CONCRETE TECHNOLOGY CORPORATION

Innovation and Quality Since 1951

Mr. Michael W. LaNier
 Vice President
 BERGER/ABAM Engineers, Inc.
 33301 Ninth Avenue South
 Federal Way, WA 98003-6395

Re: Modular Hybrid Pier Concrete Module Costs

Dear Mike:

I looked through the package you sent last month to Millard's attention and applied our previous cost experience to the quantities in the package. The following table contains the cost items and prices that I came up with.

I reformatted some items to match more closely the way we account for costs at CTC. Specifically, the graving dock rental is spread throughout all elements. Also, I added the pilaster concrete as a separate line item. CIP keel and deck concrete items contain all the costs for assembling the walls in the graving dock, plus the post-tensioning costs and the cost of materials for joining the modules together (but not the labor and equipment). I added precast decks as a separate line item and assumed that the pontoon decks would contain equal quantities of CIP and precast concrete.

The prices include the cost of 130pcf lightweight concrete. There is no cost included for mild reinforcing, but placement cost is included. My understanding is you will obtain the cost for stainless steel reinforcement and include it in the total.

Item	CY	MHP Unit Price	Total
Graving Dock			0
CIP Keel	940	\$1,451.30	\$1,364,222
CIP Deck	1280	\$1,451.30	\$1,857,664
PC Decks	1280	\$465.30	\$595,584
Ext Walls	549	\$551.30	\$302,664
Int long walls	657	\$525.30	\$345,122
Int trans walls	279	\$525.30	\$146,559
End Walls	210	\$1,116.30	\$234,423
Pilasters	165	\$2,375.30	\$391,925
Conc Stairs	50	\$800.00	\$40,000
Conc @ mooring	130	\$900.00	\$117,000
	5540	\$974	\$5,395,162

$$\times 4 = \$21,580,648$$

Manufacturers and Constructors of Prestressed and Precast Concrete

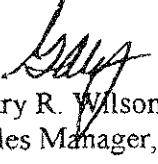
1123 Port of Tacoma Road • P.O. Box 2259 • Tacoma, Washington, USA 98401

Tacoma (253) 383-3545 • Seattle (206) 284-9611 • Facsimile (253) 572-9386 • Engineering Facsimile (253) 383-2912

I looked at the towing costs included in the package and I think they may be a little higher than necessary. I do not have a good first hand grasp on sizing of tugboats, but a 4,000 hp tug is \$325/hr (\$7,800/day) rather than \$10,000/day. Also, I am not aware of a large mobilization cost for tugboats, other than standby time and "deadhead" time if a round trip included with no backhaul.

Mike, I hope this information helps your efforts for now. If you have any questions, please give me a call.

Sincerely,
CONCRETE TECHNOLOGY CORPORATION



Gary R. Wilson
Sales Manager, Marine and Heavy Const

cc: Millard Barney, Larry Norton

Utility Costs for 1300 ft long (4 module) MHP Berthing Facility				
(all costs are installed costs - Navy construction - 2001 \$)				
Item	Units	Unit price	Quantity	Total
Structural - Per Module				
Keel Slab	1	940 CY		
Service Deck (include Crossover)	1	770 CY		
Service Deck (composite deck)	1	1 LS		
Operation Deck	1	1790 CY		
Exterior Long. Walls	1	610 CY		
Interior Long. Walls	1	730 CY		
Trans. Walls	1	310 CY		
End Walls	1	210 CY		
Mooring	1	130 CY		
Stair	1	50 CY		
				660 LF
Removal FRP Curb	1			[See Dwg S-4 S-C-1]
End Wall Barrier	1	40 LF		
High Mast Light Poles	2	POLES		[See Dwg S-3 J]
Bollards (Only Primary)	18 EA			[See Dwg S-1 J]
Form Filled Fenders (8 DIA X 14 feet)	26 EA			[See Dwg A-1 J]
Preventer Fenders	26 EA			[See Dwg S-C-1]
Cleats	48 EA			[See Dwg S-S4 S-C-1]
Misc. Pier Parts ??				
construction???				

Concrete Weight & Reinforcement

Reference dwg: S-4,S-6,S-8 [SLABS, WALLS - CONCRETE]
 S-8, S-9, S-10 [MOORING AREA]
 S-19,S-21,S-22,S-24 [P/T for SLABS & WALLS]

- Note: 1) Concrete (CY) and Reinforcement (T) are roundup to 10s.
 2) Concrete Quantities are based on the Draft Calculations
 3) S.S Reinf. Quantities are based on the preliminary Design
 (Reinforcements are not specified in the dwg.)

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Keel Slab

concrete (CY)	25202 CF	940 CY
s.s Steel (Ton)	50 kips	30 T
P/T (Ton)	155 kips	80 T

Service Deck (include Crossover)

concrete (CY)	20542 CF	770 CY
s.s Steel (Ton)	38 kips	20 T
P/T (Ton)	97.5 kips	50 T

Service Deck (composite deck)

Operation Deck

concrete (CY)	48250 CF	1790 CY
s.s Steel (Ton)	85 kips	50 T
P/T (Ton)	273 kips	140 T

Exterior Long. Walls

concrete (CY)	16333 CF	610 CY
s.s Steel (Ton)	163 kips	90 T
P/T (Ton)	29 kips	20 T

Interior Long. Walls

concrete (CY)	19624 CF	730 CY
s.s Steel (Ton)	192 kips	100 T
P/T (Ton)	0 kips	0 T

Trans. Walls

concrete (CY)	8104 CF	310 CY
s.s Steel (Ton)	52 kips	30 T
P/T (Ton)	20 kips	10 T

End Walls

concrete (CY)	5615 CF	210 CY
s.s Steel (Ton)	40 kips	20 T
P/T (Ton)	13 kips	10 T

Mooring

concrete (CY)	3460 CF	130 CY
s.s Steel (Ton)	35 kips	20 T

Stairs

concrete (CY)	1276 CF	50 CY
s.s Steel (Ton)	13 kips	10 T

KEEL SLAB , CIP (SEE DWG S-6) CONCRETE QUANTITY (PER MODULE)

(w/ 232'-0 PIGR)

BASED ON
DRAFT
CALCULATION

CIP KEEL SLABS	= 22,266 CF
ANCHORAGE	= 664 CF
	22,930 CF
tolerance (FORM)	592 CF
conc. density. (18%)	1357 CF
	24,879 CF
(Adjust to 325'-0)	x 1.013
	25,202 CF

(933 CY = 940' V)

 S.S. STEEL (BASED on Preliminary Design)

$$\text{TOP } As = \frac{0.156}{144} \text{ in}^2/\text{ft EW} \times 325' \times 88' = 31 \text{ CF}$$

$$\times 88' \times 325' = 31 \text{ CF}$$

$$\text{BOT } As = \frac{0.096}{144} \text{ in}^2/\text{ft EW} \times 325' \times 88' = 19 \text{ CF}$$

$$\times 88' \times 325' = 19 \text{ CF}$$

$$\text{TOTAL} = 100 \text{ CF}$$

$$\times p = 490 \frac{\%}{\text{CF}}$$

$$W = 49 \text{ kips}$$

$$(\approx 25 \text{ T})$$

con't KEEL SLAB (see DWG S-20)

P/T $0.6 \phi A_s = 0.217 \text{ in}^2$

$$\begin{array}{lclcl} \text{LONG.} & 17 - 12 \text{ strands} & \times 330 \text{ ft} & = & 101 \text{ CF} \\ & 17 - 12 \text{ strands} & \times 330' & = & 101 \text{ CF} \end{array}$$

$$\begin{array}{lclcl} \text{TRANSV} & 1 - 12 \text{ strands} & \times 88' & = & 16 \text{ CF} \\ & 166 - 4 \text{ strands} & \times 88' & = & 88 \text{ CF} \\ & 14 - 4 \text{ strands} & \times 68' & = & 5.7 \text{ CF} \\ & 30 - 4 \text{ strands} & \times 88' & = & 16 \text{ CF} \\ & 1 - 12 \text{ strands} & \times 88' & = & 16 \text{ CF} \end{array}$$

$$\text{TOTAL} = 316 \text{ CF}$$

$$\times p = 490^{16}/\text{CF}$$

$$WT = 155 \text{ kips}$$

$$(\approx 80 \text{ T})$$

SERVICE DECK

(SEE DNG S-4 & S-6)

(323'-0 PONTOON)

CONCRETE QUANTITY

BASED ON
DRAFT
CALC'S

SLAB = 15,558 CF

END THICKENING (CROSSOVER) = 2,598 CF

ANCHORAGE AREA (CROSSOVER) = 671 CF

18,827 CF

tolerance 320 CF

conc. density (15%) 1131 CF

20,278 CF

(Adjust to 325'-0) x 1.013

20,542 CF

(761 CY = 770 CY)

S.S. STEEL (BASED ON Preliminary Design)

$$\text{TOP } As = \frac{0.12 \text{ in}^2/\text{ft}}{144} \quad \sim 24' \times 2 = 48' \times 325' = 13 \text{ CF}$$

$$325' \times 48' = 13 \text{ CF}$$

$$\text{BOT } As = 0.24 \text{ in}^2/\text{ft} \quad 48' \times 325' = 26 \text{ CF}$$

$$325' \times 48' = 26 \text{ CF}$$

78 CF

$$\times \rho = 490 \text{ lb/CF}$$

$$WT = 38,1 \text{ k}$$

$$(T = 20 T)$$

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con't SERVICE DECK (see DWG S-19)

P/T $0.6\phi \quad A_s = 0.217 \text{ in}^2$

LONG 1 11-12 strands $\times 325'$ \approx 65CF
 11-12 $\times 325'$ \approx 65CF

TRANSV. 18 - 4 strands $\times 88'$ \approx 9.5CF
 174 - 4 strands $\times 48'$ \approx 50 CF
 18 - 4 strands $\times 88'$ \approx 9.5CF

$$\begin{array}{r} 199 \text{ CF} \\ \times \rho = 490 \text{ '9 CF} \\ \hline W = 97.5 \text{ kip} \\ \approx (50 \tau) \end{array}$$

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OPERATION DECK

(See DWG S-4 & S-6)

□ CONCRETE QUANTITY

DECK	= 38,973 CF
SLAB THICKENING	= 394 CF
END THICKENING	= 3,534 CF
ANCHORAGE	= 1,499 CF
	<hr/>
	44,400 CF
- tolerance	592 CF
- conc. tolerance (35%)	2639 CF
	<hr/>
	47,631 CF
(Adjust to 325'-0")	× 1.013
	<hr/>
	48,1250 CF
	(1787 CY ≈ 1790 CY)

□ S.S STEEL (BASED ON Preliminary Design)

$$\text{TOP As} = \frac{0.252 \text{ in}^2/\text{ft}}{144} \times \frac{\#}{325'} \times \frac{L}{88'} = 50 \text{ CF}$$

$$\times 88' \times 325' = 50 \text{ CF}$$

$$\text{BOT As} = \frac{0.18 \text{ in}^2/\text{ft}}{144} \times \frac{\#}{325'} \times \frac{L}{88'} = 36 \text{ CF}$$

$$\times 88' \times 325' = 36 \text{ CF}$$

$$\text{TOTAL} = 172 \text{ CF}$$

$$\rho = 490 \text{ lb/CF}$$

$$W_f \geq 85 \text{ kips}$$

$$(\text{say BOT})$$

Project UHP PH II
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concrete OPERATION DECK

(SEE DWG S-19)

PT

$$0.6\phi A_s = 0.217 \text{ in}^2 = 1.507 \times 10^{-3} \text{ ft}^2$$

TRANSV.

1-12 strands	$\times 88'$	= 1.59 CF
20-7 strands	$\times 88'$	= 18.6 CF
40-4 strands	$\times 68'$	= 16.4 CF
220-4 strands	$\times 88'$	= 116.7 CF
36-4 strands	$\times 88'$	= 19.1 CF
1-12 strands	$\times 88'$	= 1.59 CF

Long

$$32-12 \text{ strands } \times 330' = 191 \text{ CF}$$

$$32-12 \text{ strands } \times \underbrace{330'}_{\text{to account for diagonal part}} = 191 \text{ CF}$$

$$\text{TOTAL} = 556 \text{ CF}$$

$$\times P_{STEEL} = 490^{lb}/CF$$

$$WT = 272.4 \text{ kips}$$

$$= 136.2 \text{ Ton}$$

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LONG. WALLS

(See DWG S-4 & S-6)

EXTERIOR

□ Concrete

$$8075 + 8.102 + 430 + 397 - 2021 = 14,983 \text{ CF}$$

$$\text{Anchorage } C11+11 = 22 \quad 22 \text{ CF}$$

$$\text{CORNER BTW T&L WALL} \quad \frac{49 \text{ CF}}{15054 \text{ CF}}$$

$$\text{Tolerance } (74\% \frac{\text{CF}}{2}) = 373.5 \text{ CF}$$

$$\text{conc. density} = (12\%) \quad .905 \text{ CF}$$

$$16,333 \text{ CF}$$

$$(605 \text{ CY} \approx 610 \text{ CY})$$

1. □ S.S. STEEL

$$\star A_s = 0.12 \text{ in}^2/\text{ft EW} \quad 28' \times 2 = 56' \times 325' = 15 \text{ CF}$$

$$325' \times 2 = 650' \times 28' = 15 \text{ CF}$$

$$\text{TOTAL} = \frac{30 \text{ CF}}{x 490 \frac{1}{4} \text{ CF}}$$

$$WT = 15 \text{ kips}$$

$$\star 1\frac{3}{8}'' \text{ Ø ROD @ 18''} \quad 1\frac{3}{8}'' A_s = 1.5 \text{ in}^2$$

$$325'/1.5' \approx 217 \text{ bars}$$

$$(217 \text{ bars})(28' + 17') \left(\frac{1.5 \text{ in}^2}{144} \right) = 51 \text{ CF}$$

$$\frac{x 490 \frac{1}{4} \text{ CF}}{WT = 25 \text{ K}} \quad \nearrow 40 \text{ k}$$

$$(20T) \quad (\text{Equiv. } 2.4 \text{ pcf conc})$$

SEEMS SMALL

LET'S Assume same as Int Long. WALL.

say Equiv 10pcf conc = REINF

$$\therefore (16,333 \text{ CF}) (10 \text{ pcf}) = 163.3 \text{ Kips}$$

$$\frac{1000}{\cong (say 90 \text{ T})}$$

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(Exterior Long. WALL cont)

(See S-24 & S-27)

P/T 0.6ϕ $A_s = 0.217 \text{ in}^2$

4 strands @ 18' SPA

$\frac{1}{2}$ FULL L
 $\frac{1}{2}$ HALF L

$$325'/1.5' = 217 \text{ sets} \times 2 = 434 \text{ sets} \quad \checkmark$$

$$(434 \text{ sets})(4 \text{ strands}) \left(\frac{0.217 \text{ in}^2}{144} \right) \left(\frac{23' + 17'}{2} \right) = 59 \text{ CF}$$

$$\begin{aligned} \frac{x P = 490 \text{ kip}}{W T = 29 \text{ k}} \\ (\approx 20 \text{ T}) \end{aligned}$$

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Long. WALL

(see Dwg. S-4 & S-6)

INTERIOR

□ CONCRETE

$$6,377 + 4,633 + 5547 + 287 + 576 = 17,425 \text{ CF}$$

$$\text{ENDTHICKENING (MID WALL)} = 703 \text{ CF}$$

$$\text{Anchorage} = 67 \text{ CF}$$

$$18195 \text{ CF}$$

$$\text{Tolerance } (747 \text{ CF/2}) = 373.5 \text{ CF}$$

$$\text{conc. density (141.)} = 1035 \text{ CF}$$

$$19,624 \text{ CF}$$

$$(727 \text{ CF} = 730 \text{ CF})$$

□ S.S. STEEL

$$0.5 \text{ in}^2/\text{ft EW} \times (29' \times 6) \times 325' = 19.6 \text{ CF}$$

$$\times (325' \times 6) \times 29' = 196 \text{ CF}$$

$$\text{TOTAL} = 393 \text{ CF}$$

$$\times \rho = 490^{10} \text{ CF}$$

$$WT = 192 \text{ kips}$$

$$(100 \text{ T})$$

TRANS. WALLS (See DWG S-4)

□ CONCRETE QUANTITY

WALLS

= 5,269 CF

ADDITIONAL WALLS

= 2,166 CF

7,435 CF

Tolerance

217 CF

conc. density (6%)

452 CF

8,104 CF

(300 CY)

□ S.S. STEEL

Assume 7pcf = Δ_{STEEL}

$$(7435 \text{ CF}) (7\text{pcf}) / 1000 = 52 \text{ kips} \approx 26 \text{ T} \\ \approx 30 \text{ T}$$

(similar to DWG S-21)

□ P/T $A_s = 0.6\phi = 0.217 \text{ in}^2$

VERT. ONLY EXT: $9 \times 15\text{-}4 \text{ strands} \times 17' = 14 \text{ CF}$

(According to Marcus W.) MID: $3 \times 28\text{-}4 \text{ strands} \times 28' = 14 \text{ CF}$

EXT: $9 \times 15\text{-}4 \text{ strands} \times 17' = 14 \text{ CF}$

$$\text{TOTAL} = 42 \text{ CF} \\ \times p = 490 \frac{\text{lb}}{\text{CF}}$$

$$(\sim 3 \text{ pdt}) \quad WT = 21 \text{ kips} \\ (\sim 10 \text{ T})$$

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END WALLS

(See S-8, S-21)

CONCRETE QUANTITY

ANCHORAGE AREA = 5.615 CF

(208CY = 210CY)

SS. STEEL

Assume 7pcf = Δ STEEL

(5615CF) (7pcf) / 1000 = 39kip ≈ 40K
 = 20T

P/T 0.6φ As=0.217 in² (see DWG S-21)

VERT. 2x 15-4 strands × 17' = 3.0CF

2x 28-4 × 29' = 10CF

2x 15-4 × 17' = 3.0CF

HORIZ 2x 6-6 strands × 88' = 10CF

ʃ

2sides

TOTAL = 26CF

× p = 490 10/CF

WT = 13 kips

(≈ 10T)

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MOORING AREA

(see S-8, S-9)

CONCRETE QUANTITY

Removal + ADDITION Mooring Area = 3,145 CF

Adjustment for changing Mooring DIM
 $\frac{= 1.10}{3460 CF}$
 $(1280 Y \approx 1300 Y)$

SS STEEL

Assume 10pcf = A'Δ

$3460 (10pcf) / 1000 = 35^k \approx 20T$

STEEL COVER RE

$26' \times 26' - 11.5' \times 11.5' = 544 sf$

FENDERS

TRANSV. FENDER (MV1450X1500)

2 TRELLEX

Long. FENDER (MV1450X1000)

2 TRELLEX

2 surface RE

SHIMS

1" - RE

9

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STAIR

(see DNLG S-8)

D CONCRETE QUANTITY

REMOVAL + ADDITION = 1,215 CF

Adjusting change of Stair DM

= x 1.05

1276 CF

(47CY = 50CY)

B . S.S.

Assume 10pcf = Δ_{ss}

$(1276 \text{ CF}) (10 \text{ pcf}) / 1000 = 13 \text{ kips}$

(say 10T)

SLAB THICKENING	
y	24'-0" to 21'-0" EXT (A end)
y	24'-0" to 21'-0" EXT (B end)
y	24'-0" to 21'-0" INT (A end)
y	24'-0" to 21'-0" INT (B end)
y	21'-0" to 16'-0" EXT_Audite (A end)
y	21'-0" to 16'-0" EXT_Middle (B end)
y	21'-0" to 16'-0" EXT_Auds (A end)
y	21'-0" to 16'-0" EXT_Ends (B end)
y	21'-0" to 16'-0" INT_middle (A end)
y	21'-0" to 16'-0" INT_Ends (B end)
y	21'-0" to 16'-0" INT_Ends (A end)
y	21'-0" to 16'-0" INT_Ends (B end)
END THICKENING	
y	Top Deck
y	Mid Long Wall
y	Service Stab @ Cross Over
ANCHOR/BRACE/SEAL/PLATE	
y	Keel Stab
y	service slab
y	Top Deck
y	Boss @ Bottom
y	Boss @ Top
y	End Wall @ Top
y	End Wall @ Bottom
y	Ext Tension Wall 1
y	Ext Tension Wall 2
y	Int Tension Wall 1
y	Int Tension Wall 2
y	Int Travel Wall 1
y	Int Travel Wall 2
y	Haunch for End Ext Wall @ Top
y	Haunch for End Ext Wall @ Bottom
y	Haunch for End Ext Wall @ Top
y	Haunch for End Ext Wall @ Bottom
y	Haunch for End Int Wall @ Top
y	Haunch for End Int Wall @ Bottom
y	Haunch for End Int Wall @ Top
y	Haunch for End Int Wall @ Bottom
y	Haunch for End Long Wall (middle)
y	Haunch for Boss & Long Wall (end,top)
y	Haunch for Boss & Long Wall (end,bot)
ADDITIONAL CONCRETE (STWC)	
y	Operation Deck Removal sect 1
y	Operation Deck Removal sect 2
y	Operation Deck Removal sect 3
y	Operation Deck Removal sect 4
y	Mid Long Wall Removal
y	Side to Long Wall Removal
y	Long Wall Added (Start to Open)
y	Long Wall Added (Bottom)
y	Mid Long Wall Added (Bottom)
y	Travel Wall Added
y	Travel Wall Added 2
y	Chair added
y	Chair Lateral Slab added
y	Star Tower Long Wall
y	Star Tower Fenders Wall
y	Star Tower Ceiling
y	ADDITIONAL CONCRETE (Mounting)
y	Operation Deck Removal A
y	Operation Deck Removal B
y	Keel Stab Removal A
y	Keel Stab Removal B
y	Long wall Removal_Upper
y	Long Wall Removal_Launch
y	Long Wall Added_Upper
y	Long Wall Added_Down
y	Travel Wall_Upper
y	Travel_Wall_Seat
y	Service deck addition
y	Native Senk Disk for opening
y	Short Log Wall Blue Mounting Star
y	Local Thickening For Fenders (1)
y	Local Thickening For Fenders (2)

**MISCELLANEOUS STRUCTURES & EQUIPMENT ALLOWANCE
*** BY OTHERS *****

THE CHURCH AND THE STATE | AN ECONOMIC STUDY OF FREE AND EQUAL

WEIGHT AND CG - MISCELLANEOUS STRUCTURES AND EQUIPMENT

YAFIT

NORTH



Plan - Pontoon Related Cells

PONTOON - DELIVERY VOYAGE - TRANSPORT 2

TOTAL WEIGHT AND CENTER OF GRAVITY		WEIGHT [kips]	CRAFT [ft.]	Xo [feet]	Zo [feet]	Wx [kip-ft.]	Wy [kip-ft.]
Weights and Moments [Dg 2 & Dg 4]		20.486				901.372	3,366,548
Center of Gravity		53.258	24.00	101.50	16.78		329,238

HYDROSTATIC PROPERTIES

Floating Weight = 19.477 kips Ave. Draft due to Pontoon Wh = 10.71 ft Displacement = 304,323 cu ft
 Misc Structures and Equipment Weight = 860 kips Ave. Draft from Misc Str. & Equ Wh = 0.39 ft Displacement = 9,376 cu ft
 Ballast = 409 kips Ave. Draft due to Ballast = 0.28 ft Displacement = 6,395 cu ft
Total Weight = 20.486 kips Average Total Draft = 11.26 ft Displacement = 320,084 cu ft

Load To Sink Pontoon 1 = 161.59 kips per inch

Freeboard at Delivery Voyage = 17.62 ft

METACENTRIC HEIGHT CALCULATION - UNBALANCED

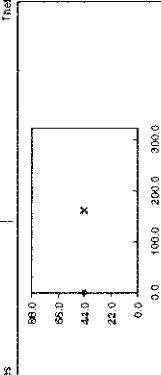
X-AXIS (Wear Dist)

KB = 5.52 ft (Center of Buoyancy to Keel)	KB = 6.62 ft (Center of Buoyancy to Keel)
BM = 68.47 ft (Center of Buoyancy to Metacenter)	BM = 767.76 ft (Center of Buoyancy to Metacenter)
XM = 65.90 ft (Keel to Metacenter)	KM = 793.28 ft (Keel to Metacenter)
KG = 15.04 ft (Keel to Center of Gravity)	KG = 18.04 ft (Keel to Center of Gravity)

GM = 47.96 ft (METACENTRIC HEIGHT)

Moment to Heel 1 = 912 kip-ft

Mx = (14) kip-ft	My = 63 kip-ft
Tan X = -0.01 in	Tan Y = 0.01 in
Theta X = 0.00 degrees	Theta Y = 0.00 degrees

**STATIC CHECK**

Joining Cost for 1300 ft long (3 joints) MHP Berthing Facility - BERGER/ABAM Baseline Estimate

(all costs are installed costs - Navy construction - 2001 \$)

Item	Units	Unit price	Quantity	Total	Comments
Labor and Equipment Costs for 1 joint					
Clean joint for joining	shifts	\$7,500	1	\$7,500	Allocate cost of \$100,000 rental over 3 joints
Rental of winch barge	LS	\$33,000	1	\$33,000	
Harbor tug assist -	days	\$6,000	10	\$60,000	per 24 hour day
Workboat and operator assist	days	\$2,500	10	\$25,000	
Position Modules, Attach tension tie, Ballast, and Dewater	Shifts	\$7,500	3	\$22,500	Crew of 1 Supv and 8 Iron workers
Remove plugs, install 435 joint bars, snug bars.	Shifts	\$7,500	6	\$45,000	3 shifts for 2 days @ 1 staff hour per bar
Grout joint	Shifts	\$7,500	4	\$30,000	1 day with 2 shifts
Stress bars	Shifts	\$7,500	6	\$45,000	2 shifts for 3 days (1 hr per bar)
Finish joint	Shifts	\$7,500	6	\$45,000	1 shift for 3 days (.5 hr / bar)
Rent Misc equipment	LS	\$50,000	1	\$50,000	Grout pump, stressing jacks,
Costs for completing 1 joint				\$363,000	
Costs for completing 3 joints				\$1,089,000	



5209 EAST MARGINAL WAY S. • SEATTLE, WA 98134 • (206) 762-0850
 MAILING ADDRESS: P. O. BOX 24067 • SEATTLE, WA 98124-0067
 WA CONTRACTOR'S LICENSE #MANSOCC032M1 • FAX (206) 764-8595

Memorandum

To: Michael Lanier, Berger / ABAM Engineers

From: Bill Shorey, Manson Construction

Ref: Modular Hybrid Pier, U.S. Navy

Per your request Manson Construction has completed a preliminary cost estimate for the module integration and the mooring dolphin elements. The documents used for this estimate are the text and drawings included in the Phase 2 Preliminary Design Report for the Modular Hybrid Pier.

Due to the preliminary nature of the drawings some interpretation was done to develop the cost of the two elements of work. The breakdown of these costs is as follows:

Module Integration:

		SAY 50% OF MATEL INCL IN CTC MODULE \$
Materials (Per Joint):	X3	\$180,000
Labor, Equipment, Supplies & Subs (1 st Joint):		\$486,000
Labor, Equipment, Supplies & Subs (2 nd or 3 rd Joint):	X2	\$324,000
		<u>270,000 FOR 3 JOINTS.</u>
		<u>486 000</u>
		<u>324 000</u>
		<u><u>324 000</u></u>
Total Cost to Integrate Modules =		<u>\$ 1,404,000 USE.</u>

The lower cost to integrate the 2nd and 3rd joints is due to the reuse of provisions and supplies on the following joint integrations.

Mooring Piers:

Materials (Per Pier):	\$585,000
Labor, Equipment, Supplies & Subs (1 st Pier):	\$1,650,000
Labor, Equipment, Supplies & Subs (2 nd Pier):	\$1,150,000

Total Cost for Two Mooring Piers = \$3,970,000

The lower cost for the second pier is due to the reuse of provisions and supplies.

The mooring piers will be very difficult to construct. Dewatering the cofferdam is not practical with the procedure as shown on the plans. The weights that would have to be added to resist the uplift load are very large. Possibly some depth can be added to the pile cap to allow a first stage concrete tremie pour that can engage the piles to the pile cap and resist the uplift.

LONG BEACH OFFICE
 1617 Pier D Street
 Long Beach, California 90802
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 California License # A-220319



SAN FRANCISCO OFFICE
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 Fax (510) 232-4528
 California License # A-220319



Berger / ABAM Engineers

August 3, 2001

Page 2 of 2

Alternatively it might be better to revise the design and use a large mono-pile cantilevered out of an excavated caisson to serve as the mooring mast. A large diameter caisson can be driven into the ground and the mooring shaft anchored inside of it. This will allow adjustment to get the accurate positioning of the mooring shaft.

The costs shown above include markup for overhead and profit. However mobilization costs are not included. It is recommended that some contingency be added to the above prices due to the preliminary nature of the design.

If you have any questions or need additional information please call.

Sincerely,

A handwritten signature in black ink, appearing to read "William Shorey".

William Shorey, P.E.

Mooring Costs for 1300 ft long (4 module) MHP Berthing Facility					
(all costs are installed costs - Navy construction - 2001 \$)					
Item	Units	Unit price	Quantity	Total	Comments
MHP MOORING COST					
Mooring Area					
Sliding Steel Cover PL	544 SF	\$15.30	1	\$8,323	
				TOTAL	\$8,323
Fendering					
T. Trelllex Fenders (MV1450x2000)	4 EA	\$3,500.00	1	\$14,000	
L. Trelllex Fenders (MV1450x1000)	4 EA	\$1,750.00	1	\$7,000	
Surface PL (MV1450x2000 A)	2 EA	\$11,400.00	1	\$22,800	
Surface PL (MV1450x1000 B)	2 EA	\$4,000.00	1	\$8,000	
9-Shims (MV1450x2000)	2 SIDES	\$20,700.00	1	\$41,400	
9-Shims (MV1450x1000)	2 SIDES	\$10,800.00	1	\$21,600	
				TOTAL	\$93,200
Guided Shaft					
Steel shafts (including ht. PL and End PL)	74000 lb	\$1.80	1	\$133,200	
INT. PL	70000 lb	\$1.80	1	\$126,000	
END PL	14000 lb	\$1.80	1	\$25,200	
1.5" dia Vertical Bars (4)	41 LF	\$30.00	4	\$4,920	
				TOTAL	\$289,320
Pile Cap					
Precast	80 CY	\$366.00	1	\$29,280	not installed
Cast-in-place	150 CY	\$373.00	1	\$55,950	installed
GROUT	10 CY	\$373.00	1	\$3,730	installed
				TOTAL	\$88,960
Precast Piles					
20" oct. pile- 22 strands	100 LF	\$55.00	16	\$88,000	installed (Ref: Prev. project)
				TOTAL	\$88,000

Mooring Costs for 1300 ft long (4 module) MHP Berthing Facility					
(all costs are installed costs - Navy construction - 2001 \$)					
Item	Units	Unit price	Quantity	Total	Comments
Leveling System					
Steel Leveling Cap	9000 lb	\$1.50	1	\$13,500	
Leveling Screws	8 EA	\$15.00	1	\$120	
1.5" High Strength Bars w/ embed anchor	6.5 LF	\$30.00	8	\$1,560	
Embed PL (Steel) - machine segregated	11760 lb	\$5.00	1	\$58,800	
Sliding PL (Steel) - machine segregated	11760 lb	\$5.00	1	\$58,800	
Extra Concrete to cover the plates	5 CY	\$373.00	1	\$1,865 installed	
		TOTAL		\$134,645	
Construction					
Sheet Pile					
Dewatering					
Temporary Shoring					
Temp Anchors					
Temp Bracing					
Pile Load Test?					
SUBTOTAL FOR MHP MOORING				\$ 1,002,448	PER MOORING
X 2 moorings				\$ 2,004,896	For 1300 Foot Pier

Project MHP PHII
Sheet _____ of _____
Subject COST ESTIMATE
Job Number A01047
MOORING
Designer KAP
Date 6/29/01

► MOORING AREA

- PRECAST CONCRETE \Rightarrow PART of MHP MODULE
- SLIDING STEEL COVER RE (DWG DETAIL 3 of 5-5)
 - 26'x26' OUTER - 11.5'x11.5' inner = 544SF
say $\frac{3}{8}$ " RE

$$VOL = (544SF) \left(\frac{\frac{3}{8}}{T2} \right) = 17CF$$

$$WT = (17CF)(490 \text{ lb/CF}) = 8,326 \text{ lb}$$

- COST

Means P189
W27x114 \Rightarrow ~60¢/lb STEEL (SEE GUIDE SHIFT)

i. say unit cost \$1.00/lb.

$$\underline{\underline{COST = \$ 8,326}}$$

$$\left[\begin{aligned} \text{unit cost (SF)} &= \frac{\$8,326}{544SF} \\ &= \$15.32/SF \end{aligned} \right]$$

Project MHP PHII
Subject COST ESTIMATE
MOORING

Sheet _____ of _____
Job Number A01047
Designer KAP
Date 6/29/01

► FENDERING (DWG. 3/S-9)

- T. TRELLEX FENDER MV 1450x2000 - (476'x6.56')
- L. TRELLEX FENDER MV 1450x1000 - (4.76'x328')

- Per Mike

FORM FILLED FENDER ≈ \$540/FT

Let's assume

$$\text{MV } 1450 \times 2000 \Rightarrow \$540/\text{ft} \times 6.56' = \$3,542 \\ \approx \$3,500/\text{EA}$$

$$\text{MV } 1450 \times 1000 \Rightarrow \$3,500/2 = \underline{\$1750/\text{EA}}$$

BERGER/ABAM
ENGINEERS INC.

Project MHP PHIL
Sheet _____ of _____
Subject COST ESTIMATE
Job Number A01047
Designer KAP
Date 6/29/01

- SLIDING TE. (Surface TE) — (see DWG. 3/39, 1/58)

SIZE \approx 76" x 105"

↑
1133 (2000 mm)

MV1250

1133 (1250 mm)

TE WIDTH \approx 1660 mm
 \approx 66"

MV1000

1133 (1000 mm)

WIDTH \approx 1330 mm
 \approx 52"

○○ MV1450

W \approx 1932 mm

\approx 76"

REF TREUXX Manual (attached)

P920 PANEL WT (w/o chane)

assume

ORIENTATION = VERTICAL (Fig 3)

$$H = MV1450 = 1450 \text{ mm} = 1.450 \text{ m}$$

$$L = 2000 \text{ mm} = 2.0 \text{ m}$$

compound A

$$\max WV = 2.0 \times 1.78 \times 1.45 = 5.1 \text{ tonnes} \approx \boxed{11,380 \text{ lb}}$$

LET'S assume W = 11,400^{lb}

unit cost \$1.00/lb

MV1450 x 2000

COST = \$11,400/PANEL

• MV 1450x1000

$$\text{max } W_V = 1.0 \times 1.25 \times 145^m = 1.81 \text{ tonnes} = 3995 \text{ lb}$$

compound (B)

$$H = 1.45m$$

$$L = 1m$$

$$\text{unit cost} \rightarrow \$1/\text{lb}$$

$$\boxed{\text{MV 1450x1000 COST} = \$4000 / \text{panel}}$$

- Shims (DWG 1/S-B) (Similar to panel size)
1" P
 - Shims located BASE of MHP SIDE of FENDERS
 - Assume 9 - 1" shim PLATE

Let's assume size shims as follows.

$$\text{MV 1450x2000} \rightarrow 76" \times 106" \quad A = 56 \text{ SF} \quad V = 4,664 \text{ WT} = 2283 \text{ lb}$$

$$\text{MV 1450x1000} \rightarrow 76" \times 53" \quad A = 28 \text{ SF} \quad V = 2,334 \text{ WT} = 1141 \text{ lb}$$

$$\text{unit cost} = \$1.00/\text{lb.}$$

$$\therefore \text{MV 1450x2000}$$

$$\underline{\$2,300/\text{sht} \times 9} = \$20,700$$

$$\text{MV 1450x1000}$$

$$\underline{\$1,200/\text{sht} \times 9} = \$10,800$$

STEEL PANELS

The *Trellex Steel Panel* is a closed box design as standard and is developed for maximum strength at minimum weight. Plain and smooth outer surfaces guarantee the best treatment and control of the marine corrosion protection and minimize the exposed surface area. The grade of steel depends on requirement and is calculated for every customized case. Normally used grade of steel is stronger than 43 A (ASTM A 36 or JIS 3101), which is minimum grade used. Example of different types of panels, multiple fenders and special fenders, see pages 26-27.

FENDER PANELS WITHOUT WEIGHT CHAINS

A considerable amount of permanent weight can be supported by the MV elements.

Maximum allowed permanent weight W of panel to be supported by the MV elements only is dependent on element sizes (H and L) and compound of rubber (A or B).

H = size in m (example MV 750; $H = 0.75$ m)

Table below can be used for calculating allowed weight of panel without weight chains. It shows the weight which can be supported by a pair of MV elements 1 metre in length (L) orientated vertically (W_v , fig. 3) or horizontally (W_h , fig. 4).

Combining weight W_v and W_h can be applied.

Compound A		Compound B	
W_v	W_h	W_v	W_h
1.78 H	1.0 H	1.25 H	0.7 H
Weight in tonnes			

Example:

Two vertical orientated MV elements MV 750 x 1500 A and two horizontal MV 750 x 1000 B behind a panel.

Weight of panel to be supported by MV elements only may not exceed W total.

$$W \text{ total} = 1.5 \times 1.78 \times 0.75 + 1.0 \times 0.7 \times 0.75 = 2.53 \text{ Tonnes}$$

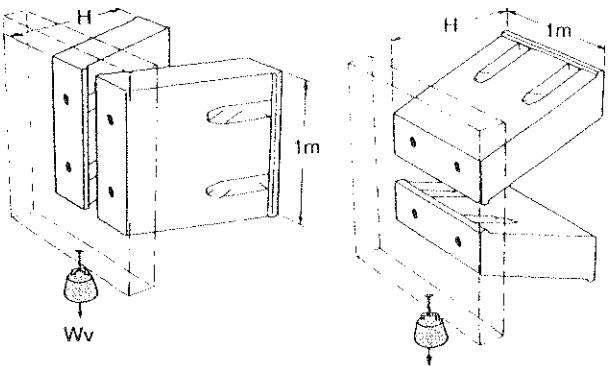


Fig. 3

Fig. 4

Marine corrosion protection can be according to BSI, ASTM, SIS or other standards applicable.

Open-Grid-design for hot dip galvanizing can be made as an alternative, but will result in heavier panels.

As shown below there are great advantages in designing light panels and use of low friction facing. Weight chains and/or shear chains can in many cases be avoided.

FENDER PANELS WITHOUT SHEAR CHAINS

The fender elements are often able to transfer the momentary transversal forces to the structure. The friction along the panel will cause a sideways deflection.

SHEAR STIFFNESS of standard MV elements

Momentary transversal deflection caused by shear forces independent of compound (A or B) and length (L).

F = Rated reaction force at deflection min. 0.27 H

C_f = Coefficient of friction (formulas valid for C_f 0-0.4)

F_f = Shear force caused by friction $F_f = F \times C_f$

D_l = Deflection longitudinal at shear force (mm)

Formula: $D_l = 0.39 \times H \times C_f$

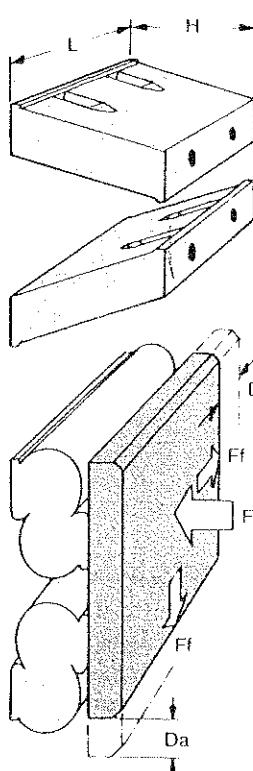
D_a = Deflection across at shear force (mm)

Formula: $D_a = 0.82 \times H \times C_f$

Example: $H = 1000$ mm (MV 1000 x ____ A or B)

$C_f = 0.2$

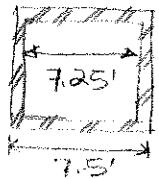
$D_l = 0.39 \times 1000 \times 0.2 = 78$ mm 3.1"



GUIDE SHAFT (DNG S9, S11)

► STEEL TUBE $L = 41\text{ft}$

$$7\text{-}6" \times 7\text{-}6" \times 1\frac{1}{2}" \Rightarrow A = 3.69 \text{ sf}$$



$$\text{VOL} = 151.2 \text{ CF}$$

$$\text{WT} = 151.2 \text{ CF} \times 490 \text{ lb/CF}$$

$$L \approx 41\text{ft}$$

$$(\text{assume } 10\text{P}) = 74,088 \text{ lb} = 74\text{k}$$

$$\circ \text{ INT. IR} = 7.5 \times 7.5 \times \frac{1}{4} " = 14 \text{ CF} \rightarrow 7\text{k} \times 10\text{P}$$

$$\circ \text{ END IR} = 7.5 \times 7.5 \times 1\frac{1}{2} " = 28 \text{ CF} \rightarrow 14\text{k}$$

(MEANS P139)

$$\boxed{\text{TOTAL} = 158\text{k}}$$

W 27x14

$$\text{WT} = 14\text{k} \times 1 = 14\text{k}$$

$$= 57\text{t} \rightarrow \$ 69/\text{material}$$

MATERIAL

$$\boxed{\text{unit} = \$1.15/\text{ton}}$$

$$\text{MATERIAL cost} \approx 60 \text{¢/lb.}$$

unit cost:

say

$$\$140 \text{ to } \$180/\text{lb}$$

(w/ WELDING etc)

$$\text{COST} = (158,000 \text{ lb})(\$1.15/\text{lb}) = \$284,400 / \text{SHAFT}$$

$$(\text{unit } \$/\text{LF} = \$69.37/\text{LF})$$

• VERTICAL BARS (Dwg 3/S11 # 1/S-12)

$1\frac{1}{2}'' \phi$ High Strength Bars

LF = 41'

QUANTITY = 4

COST : similar to P/S STRANDS

per mile : Let's use \$5/lb

$$1\frac{1}{2}'' \phi \quad A = \pi(0.75'')^2 = 1.77 \text{ in}^2 = 0.0123 \text{ ft}^2$$

$$\text{VOL (ft)} = 0.00123 \text{ CF}$$

$$\text{WT} = 6.0 \text{ LB. (per 1ft)}$$

$$\therefore \text{unit cost/LF} = \$5/\text{lb} \times 6^{\text{lb}} = \boxed{\$30/\text{ft}}$$

$$\text{COST} = (41') (\$30) (4) = \boxed{\$4,920}$$

PRECAST (DWG S-11)

> PRECAST

$$VOL \approx 76CY \approx 80CY$$

(means p161)

24" x 52" x 40' BM
 ||

	<u>MAT</u>	<u>Labor</u>	<u>EQ</u>	<u>TOTAL</u>	<u>TOTAL OH</u>
\$ 4025	\$ 111	\$ 78	\$ 4214	\$ 4700	

12.84CY \$ 313/CY \$ 8.6/CY \$ 607 \$ 328. \$ 366/CY

$$\begin{array}{r} \times 80CY \\ \hline \text{BEAR COST} = \$29,280 \end{array}$$

TO PLACE ??

Project MHP PH II
 Subject COST Estimate

Sheet _____ of _____
 Job Number A01047
 Designer KAP
 Date 6/29/01

► CAST-IN-PLACE (DNG S-II)

$$VOL \approx 148 \text{ CY} = 150 \text{ CY}$$

(MEANS P161)
2001

CP 6000psi

TOTAL OH

$$\Rightarrow \$91.50/\text{CY}$$

(MEANS P158)

PLACING CONCRETE

W/CRANE BUCKET

24" thick

$$\Rightarrow \$70/\text{CY} \times 4 = \$280.$$

water
construct

$$\$372/\text{CY}$$

$$\times 150 \text{ CY}$$

$$\underline{\underline{\$55,800 IN PLACE}}$$

$\text{CAST-IN-PLACE} \approx \$56,000$ CONC
--

$$(\text{unit price} = \$373/\text{CY})$$

► GROUT

$$VOL = 10 \text{ CY}$$

$$\text{Assume unit price} = \frac{\text{CAST IN PLACE}}{\text{conc. unit price}} = \$373/\text{CY}$$

$\therefore \text{cost} = \$3730 \approx \$4,000$

Project MHP PH II
Subject COST ESTIMATE

Sheet _____ of _____
Job Number A01047
Designer KAP
Date 6/29/01

► CONCRETE PILE ^{S-9}
(Dwg S-11)

► 24" OCT. PILE

$$\begin{aligned} \text{LENGTH} &= 20' (\text{top cap to sea bottom}) + 50' (\text{embed L}) \\ &\quad + 20' (\text{top cap to watersurf}) + 5' (\text{above water, }) \\ &\approx 95' \quad \text{say } 100' \end{aligned}$$

► COST

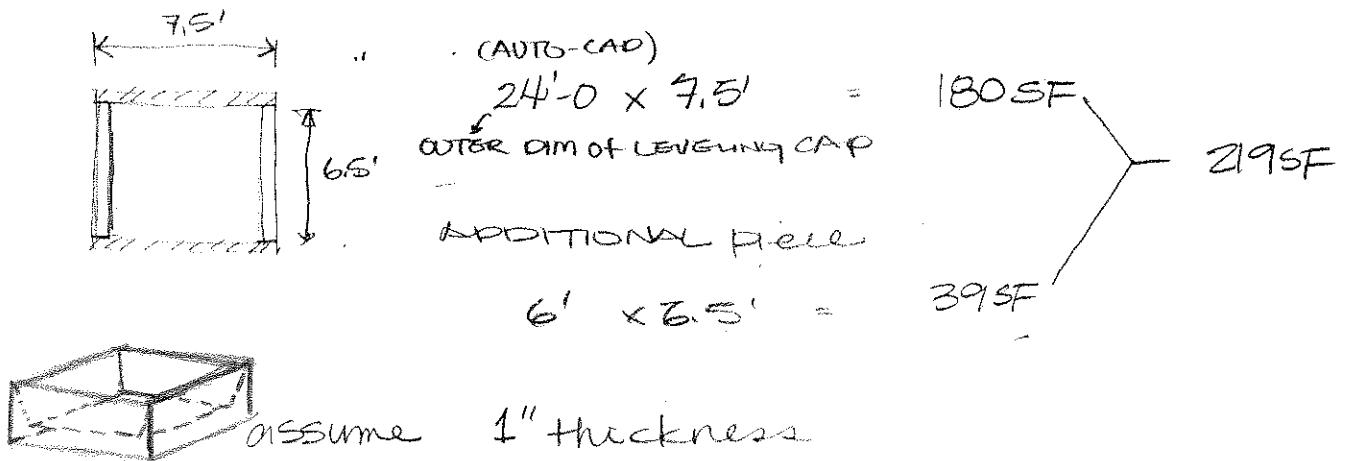
REF: Lewis K.

Hundai (?) Job Cost.

24" oct pre-cast pile → \$5/LF INSTALLED
(used 5% inflation)

LEVELING SYSTEM

► STEEL LEVELING CAP (DWG 1/S-12)



$$VA = (219 \text{ SF}) (1\frac{1}{2}) = 18.25 \text{ CF}$$

$$\begin{aligned} WT &= 18.25 \text{ CF} \times 490^{\text{lb}/\text{CF}} = 8,942^{\text{lb}} \\ &\approx 9,000^{\text{lb}} \end{aligned}$$

unit cost assume \$ 1.50

<u>COST = \$ 13,500</u>

Project MHP PH II
Subject COST ESTIMATE

Sheet _____ of _____
Job Number A01047
Designer KAP
Date 01/29/01

► GENERATE RE TOP & BOT (Dwg b-12)

$$\text{TOP } 6' \times 4' \times 3" \text{ TICK} = 6 \text{ CF} \times 490^{\text{lb}}/\text{CF} = 2940^{\text{lb}} \times 4^{\text{ft}} \\ = 11,760^{\text{lb}}$$

$$\text{BOT } 6' \times 4' \times 3" \text{ TICK} = 11,760^{\text{lb}}$$

$$\text{TOTAL WT} = 23,520^{\text{lb}}$$

COST

GROSS \$500/lb (MILE)

(unit cost = \$5/lb)

COST = \$117,600

► LAGGING SCREWS (DWG S-12)

QUANTITY → 8 EA.

(means p183)

LAG SCREWS

5/8" dia 3"

(MATERIAL + LABOR + OHA)

\$ 3.72/EA.

↓

Say 12"

\$ 15.00/EA

$$\begin{array}{r} \times 8 \\ \hline \text{COST} = \$120 \end{array}$$

$\text{COST} = \$120 / \text{CAP}$

► 1 1/2" Ø High Strength Bars (DWG S-12)

unit cost = \$30/LF (same as shaft bars)

LF = 6.5 ft.

QUANTITY = 8

unit cost = \$30/LF

$\text{COST} = \$1,560$

Transmittal Memorandum

To: Ed Blessing
7049 E Desert Spoon Ln.
Gold Canyon, AZ 85219

Date 3 July, 2001
Project Modular Hybrid Pier
Our Number A01047

Attention Ed

Phone: 480-983-7642

Regarding Cost Estimating Input

I am forwarding Modular Hybrid Pier Estimating Information

Prints Originals Reproducibles Photocopies Other

Quantity	ID Number	Date	Description
1 set		<u>July 3, 2001</u>	<u>Estimating Information</u>

Remarks Dear Ed:

Attached is the material we discussed. We would like you to concentrate on estimating the two mooring shaft support dolphins complete with mooring shaft installed. (see the installation drawing for this element) Then take a look at the floating concrete module estimate and see if you have an opinion about the cost. I am trying to get Manson to take a look at the cost of the floating concrete modules, but I would still like any input you have. I would also like your general input on how we might be able to improve the constructability of the mooring elements. There are some tolerance issues that will likely be difficult to deal with. There are differing opinions about how closely we can position the pile cap... using it as a template for driving. Give me a call at 206-431-2300 if you have any questions or want to discuss any of the features.

You mentioned that you could spare a couple of days for this. That amount of time would be about right. Please send your bill to my attention and note where you want the check sent. Thanks for your help.

Regards,



Michael W. LaNier
Vice President

CC: Kayoko Price

Mike Lanier

From: Edward Blessing [elb-mmb@worldnet.att.net]
sent: Saturday, July 07, 2001 1:11 PM
To: Mike LaNier
Subject: MHP costs / comments



cost est detail.doc



A01047-001.PUB



A01047-002.PUB

Mike,

I have estimated the Mooring Dolphins and have attached my detailed cost estimate. This certainly is a difficult structure to construct but I came up with a scheme for the precast cap support structure and cofferdam that I feel will work. They have not been "engineered" and the material sizes and costs may increase when the designs are completed. The costs do not contain a contingency for design details. As you read the detailed costs, I did not include shaft fendering which if feel Kayoko covered in her estimate.

In reviewing the floating Module costs, in my opinion, the fabrication costs appear to be adequate at \$4,500,000 ea. I think the joining costs are light and would expect a cost of at least \$250,000 per joint. As an example, each joint will require a cofferdam around the girth and the area pumped before the bolt holes are punched through.

I suggest that you include a system of mating cones where pontoon "A" has two "male" projections and pontoon "B" has matching "female" receptacles. The pontoons are winched together and, when snug, the bolt holes will be in alignment. This may add some cost to the fabrication but will save time and money in aligning and bolting.

I am attaching my detailed cost estimate for the mooring dolphins and two crude drawing of cofferdam and support structure.
I will send hard copy of the estimate and more detailed concept of cofferdam and support str.

Thank you for the work I'll call Monday (7/9/01) in the early afternoon to see if you have any questions. I'll also e-mail my time sheet to Patty.

Thanks again!

Ed Blessing

MODULAR HYBRID PIER
MOORING DOLPHIN
COST ESTIMATE DETAIL

1. Support Structure

The support structure consists of 8 ea 24" dia. x ½" wall steel pipe pile 100 ft. long placed 5' +/- each way from the corners of the precast pile cap. The piles are cutoff and capped with a steel plate and jacks placed atop the plates. Doubled 14"HP102 sections are placed between piles at each corner and raises to the proper invert elevation of the PC cap and secured. PC cap is then lowered underwater whereupon it's corners rest on the HP beams.

- 8 ea. 24"x1/2"x100' pipe = 104,000 lb. @ \$.20 = \$20,800
- Dbl. 14HP102x12"x4ea = 10,00 lb @ \$.35 = \$3,500
- Plate and bracing = \$10,700
- Jacks, 8 ea. @ \$1,000 = \$8,000

Subtotal = \$44,000

Derrick & Crew

Equipment = \$5,400 /shift
Operators = \$1,000 / shift
Pile bucks = \$ 2,600 / shift

+ \$10,00 / shift

Divers, 2 crew of \$2,00 = \$4.00 / shift

- Drive pile, 2 shift @ \$10,000 = \$20,000
- Cut off, cap, & level, 2sh. @ \$10,000 = \$20,000
- Divers, 2 shift @ \$4,000 = \$8,000

Subtotal = \$48,000

Item Total = \$92,000

2. Precast Cap

- Fabricate pc cap, 80 cy @ \$300 = \$24,000
- Guides, sling, etc. = \$6,000
- Place on support frame, 1 shift w/divers = \$14,000

Item Total = \$44,000

3. Pile Driving

16 ea. 24" octagonal x 100'

- Buy pile, 1,600' @ \$50 = \$80,000
- Drive pile, 4 shifts @ \$10,000 = \$40,000
- Cut off pile, 4 diver shifts @ \$4,000 = \$16,000

Item Total = \$136,000

4. Concrete Pile to PC Cap

- Forms = \$2,500
- Concrete = \$1,000
- Install = 1 sh w/ divers & derrick = \$14,000

Item Total = \$17,500

5. Cofferdam

3/8" steel plate walls with 4"x4"x1/4" angle stiffeners at 2'-0" o/c in each direction (like a barge hull). Sheet pile interlocks at the corners. Walls to be snug fit to outside of PC cap walls with rubber strip.

- 3/8" pl, 4 ea 30'x30' + 900' angle + misc struts and braces = 110,000 lb @ \$1 = \$110,000
- Interlocks, 120' @ \$20 = \$2,400
- Install, 1 sh. W/ derrick & diver crews = \$14,000
- Pump and seal = \$7,000

Item Total = \$133,400

6. C.I.P. Concrete 135 c.y.

- Concrete @ \$92 = \$12,420
- Ferry to site @ \$18 = \$2,430
- Reinforcing steel, 130#/c.y. @ \$65 = \$8,775
- Place @ \$75 = \$10,125

Item Total = \$33,750

7. Shaft

7.5' square x 1 1/2" plate x 41' long = 75,300 lb., + Stiffeners and top plate = 6,900 lb

- Buy steel, 83,000 lb @ \$.40 = \$33,200
- Fabricate Steel @ \$1.60 = \$132,800

Item Total = \$166,000

8. Shaft Hardware

- Vertical hold down bars, 164' @ \$30 = \$5,000
- Leveling system, 9,000 lb @ \$2 = \$18,000
- Alignment Plates, 24,000 lb @ \$4 = \$92,000
- Bolts = \$2,000

Item Total = \$117,000

9. Fit-up Shaft

- Place, plumb & brace shaft, 1 shift @ \$10,000
- Grout leveling Base = \$1,000
- Temporary supports, allow \$2,000

Item Total = \$13,000

10. Remove Cofferdam & Support Structure

- Remove Cofferdam, 1 shift @ \$14,000
- Remove support frame, 1 shift @ \$14,000
- Pull pipe piles, 2 shift @ \$14,000 = \$28,000

Item Total = \$56,000

11. Temporary pier Moorings

- Rent anchors, chain, buoys, etc. = \$10,000
- Place, moor, remove, 3 shift @ 410,000 = \$30,000

Item Total = \$40,000

12. Install Shafts

- Place & grout underwater, 1 shift @ \$14,000
- Dewater = \$1,000
- Install hold down rods = \$3,000
- Place concrete = \$5,000

Item Total = \$23,000

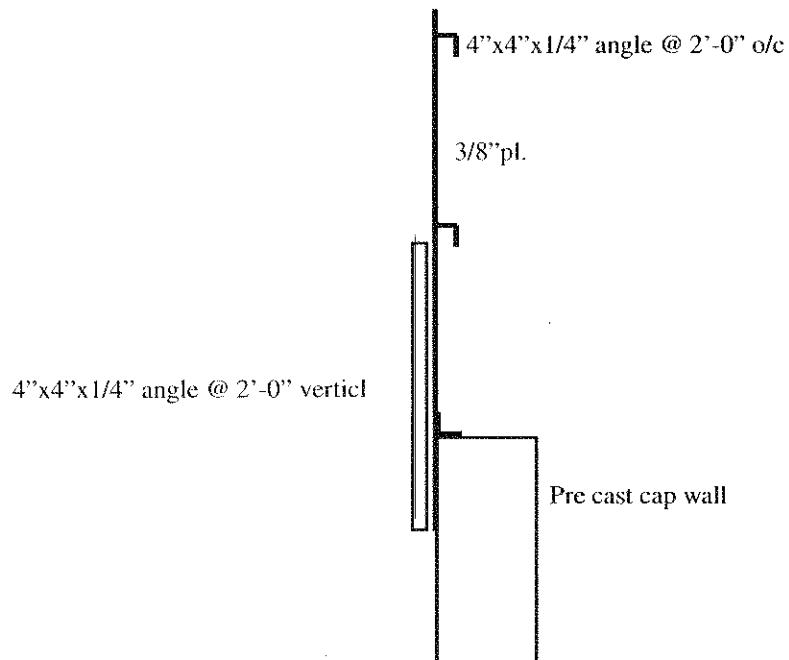
SUMMARY OF COSTS

1. Support System	\$ 92,000
2. PC Pile Cap	\$ 44,000
3. Pile Driving	\$136,000
4. Concrete Piles to Cap	\$ 17,500
5. Cofferdam	\$133,400
6. C.I.P. Concrete	\$ 33,750
7. Shaft	\$166,000
8. Shaft Hardware	\$117,000
9. Fit-up Shaft	\$ 13,000
10. Remove Temp. Const.	\$ 56,000
11. Temp Moorings	\$ 20,000
12. Install Shafts	\$ 23,000
 Subtotal	 \$851,650
20% OH & Profit	\$170,350
 TOTAL	 \$922,000 per dolphin

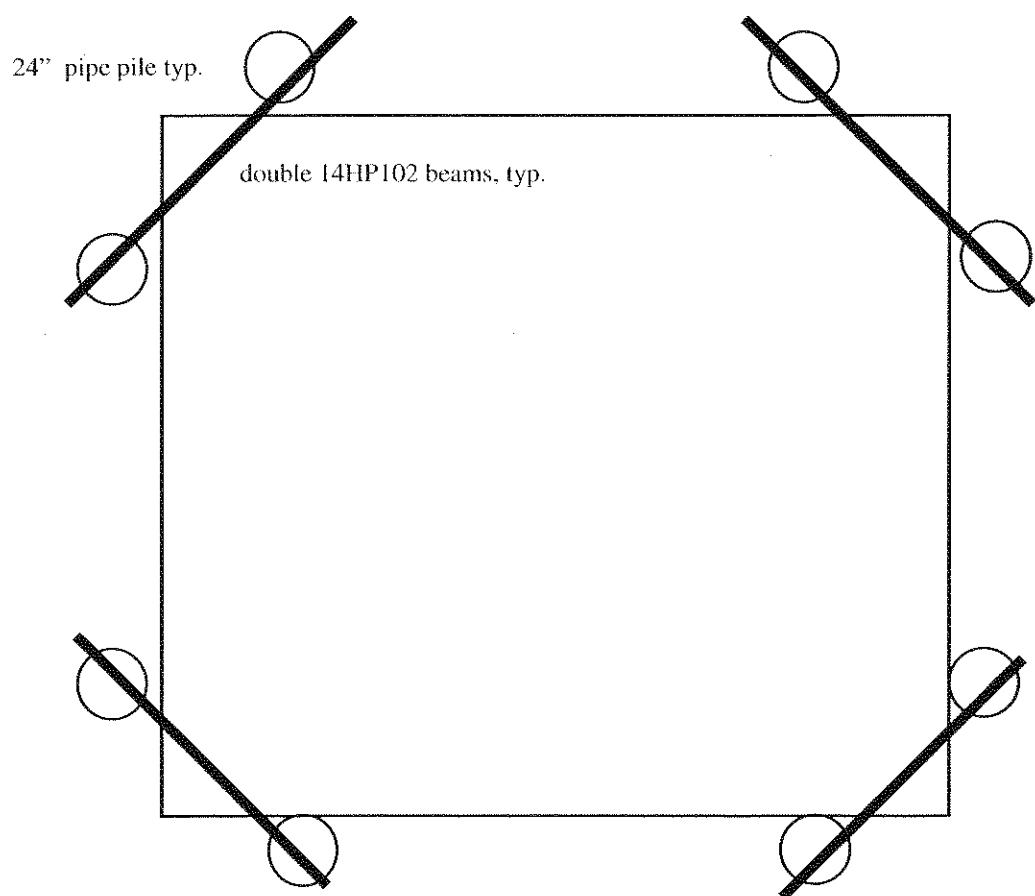
2 ea. Dolphins = \$1,844,000

Note: This estimate does not include shaft fendering attached to the floating module. Towing, mobilization, demobilization and site tug / transportation are likewise excluded except as noted. Task specific equipment is included.

COFFERDAM WALL TYPICAL SECTION



PRECAST CAP SUPPORT STRUCTURE





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Memorandum

To: Michael Lanier, Berger / ABAM Engineers

From: Bill Shorey, Manson Construction

Ref: Modular Hybrid Pier, U.S. Navy

Per your request Manson Construction has completed a preliminary cost estimate for the module integration and the mooring dolphin elements. The documents used for this estimate are the text and drawings included in the Phase 2 Preliminary Design Report for the Modular Hybrid Pier.

Due to the preliminary nature of the drawings some interpretation was done to develop the cost of the two elements of work. The breakdown of these costs is as follows:

Module Integration:

Materials (Per Joint):	X3	\$180,000	SAY 50% OF MATEL INCL IN CTC MODULE \$
Labor, Equipment, Supplies & Subs (1 st Joint):		\$486,000	270,000 FOR 3 JOINTS.
Labor, Equipment, Supplies & Subs (2 nd or 3 rd Joint):	X2	\$324,000	486,000 324,000 <u>324,000</u>
Total Cost to Integrate Modules = \$1,674,000			\$1,404,000 USE.

The lower cost to integrate the 2nd and 3rd joints is due to the reuse of provisions and supplies on the following joint integrations.

Mooring Piers:

Materials (Per Pier):	\$585,000
Labor, Equipment, Supplies & Subs (1 st Pier):	\$1,650,000
Labor, Equipment, Supplies & Subs (2 nd Pier):	\$1,150,000

Total Cost for Two Mooring Piers = \$3,970,000

The lower cost for the second pier is due to the reuse of provisions and supplies.

The mooring piers will be very difficult to construct. Dewatering the cofferdam is not practical with the procedure as shown on the plans. The weights that would have to be added to resist the uplift load are very large. Possibly some depth can be added to the pile cap to allow a first stage concrete tremie pour that can engage the piles to the pile cap and resist the uplift.

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Berger / ABAM Engineers

August 3, 2001

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Alternatively it might be better to revise the design and use a large mono-pile cantilevered out of an excavated caisson to serve as the mooring mast. A large diameter caisson can be driven into the ground and the mooring shaft anchored inside of it. This will allow adjustment to get the accurate positioning of the mooring shaft.

The costs shown above include markup for overhead and profit. However mobilization costs are not included. It is recommended that some contingency be added to the above prices due to the preliminary nature of the design.

If you have any questions or need additional information please call.

Sincerely,

A handwritten signature in black ink, appearing to read "William Shorey".
William Shorey, P.E.

Service Deck Ramp Cost - MHP Berthing Facility (all costs are installed costs - Navy construction - 2001 \$)					
Item	Units	Unit price	Quantity	Total	Comments
Ramp basic structure - installed	SF	\$145	1176	\$170,520	98 ft X 12 ft = 1176 sf
Ramp transition structure pier end	SF	\$100	36	\$3,600	3 ft X 12 ft = 36 sf
Ramp transition structure shore end	SF	\$100	252	\$25,200	12 ft X 21 ft = 252 sf
Pier end support wheel installation	LS	\$7,000	1	\$7,000	
Shore end support wheel installation	LS	\$14,000	1	\$14,000	
				25 ft X 3 ft X 5 ft = 14 cubic yd @	
Pier end support corbel	LS	\$5,500	1	\$5,500	\$800/cubic yd
Shore end abutment	LS	\$30,000	1	\$21,000	35 cubic yards @ \$600 per cubic yard
Utilities support structure	LF	\$100	120	\$12,000	
Total Cost of Service Deck Ramp				\$258,820 Baseline	
				\$245,879 Low range @ 95% of Baseline	
				\$284,702 High range @ 110% of Baseline	

Utility Costs for 1300 ft long (4 module) MHP Berthing Facility					
	Item	Units	Unit price	Quantity	Total
					Comments
Electrical					
High voltage electrical feed from on-shore electrical vault to MHP shore end	EA	\$7,769	2		\$15,538
High voltage electrical feed from MHP shore end to substations	EA	\$215,853	2		\$431,705
Electrical Substations	EA	\$531,754	8		\$4,254,031
Fixed cable feeds from substations to turtlebacks	LF	\$62	26400		\$1,632,709
Electrical Distribution Turtlebacks	EA	\$37,694	12		\$452,326
15% for misc. undesignated details	LS	\$1,017,946	1		\$1,017,946
Electrical Total					\$7,804,255
Mechanical					
MHP fixed potable water piping system	LF	\$66	3096		\$205,636
Potable water piping pressure test	HR	\$96	64		\$6,123
Potable water pipe hangers	EA	\$144	347		\$50,020
Potable water sectionalizing valves	EA	\$839	33		\$27,671
Potable water sectional flex connections	EA	\$1,081	6		\$6,486
Potable water backflow preventors	EA	\$4,034	96		\$387,288
Potable water hose connectors	EA	\$142	96		\$13,585
Potable water outlet valves	EA	\$1,326	96		\$127,336
Potable water MHP to ship hoses (per berth X no of berths)	EA	\$186	192		\$35,735
Potable water line from MHP to on-shore manhole	LF	\$66	400		\$26,568
Motion accommodations provisions MHP to shore	EA	\$6,001	4		\$24,003
Potable water on-shore hook-up	LS	\$7,365	1		\$7,365
MHP fixed compressed air piping system	LF	\$55	2968		\$163,869
Compressed air piping pressure test	HR	\$96	64		\$6,123
Compressed air pipe hangers	EA	\$144	347		\$50,020
Compressed air sectionalizing valves	EA	\$1,795	33		\$59,219
Compressed air sectional flex connections	EA	\$554	6		\$3,325

Utility Costs for 1300 ft long (4 module) MHP Berthing Facility					
	(all costs are installed costs - Navy construction - 2001 \$)			Total	Comments
Item	Units	Unit price	Quantity	Total	
Compressed air hose connectors: 1-1/4"	EA	\$102	48	\$4,918	Quick-connect fitting
Compressed air hose connectors: 1/2"	EA	\$76	48	\$3,658	Quick-connect fitting
Compressed air outlet valves: 1-1/4"	EA	\$185	48	\$8,901	SS ball valve
Compressed air outlet valves: 1/2"	EA	\$63	48	\$3,001	SS ball valve
Compressed air MHP to ship hoses (per berth X no. of berths)	EA	\$228	96	\$21,928	50' hose section w quick-connect fittings: (2) sections per manifold connection
Compressed air line from MHP to on-shore manhole	LF	\$66	400	\$26,568	Based on connection within 100' of pier
Motion accommodations provisions MHP to shore	EA	\$5,806	4	\$23,223	6" braided SS connector, 8' long w floating flange + isolation valves
Compressed air on-shore hook-up	LS	\$4,995	1	\$4,995	
MHP fixed oily waste piping system	LF	\$66	2619	\$174,143	4" / 6" double-wall FRTP pipe
Oily waste piping pressure test	HR	\$96	64	\$6,123	16 Hr per section + equipment rental
Oily waste pipe hangers	EA	\$144	296	\$42,668	Vinylester hanger w SS all-threaded rod
Oily waste sectionalizing valves	EA	\$1,795	32	\$57,424	4" ball valve
Oily waste sectional flex connections	EA	\$345	6	\$2,072	4" braided SS connector, 2' length
Oily waste hose connectors	EA	\$186	16	\$2,971	Cam-lok fitting
Oily waste outlet valves	EA	\$867	16	\$13,867	4" ball valve
Oily waste MHP to ship hoses (per berth X no. of berths)	EA	\$687	32	\$21,973	50' hose section w cam-lok fittings: (2) sections per utility connection
Oily waste mobile pumping unit	EA	\$21,510	8	\$172,083	
Oily waste line from MHP to on-shore manhole	LF	\$90	800	\$72,240	Based on connection within 300' of pier
Motion accommodations provisions MHP to shore	EA	\$4,829	4	\$19,317	4" braided SS connector, 8' long w floating flange + isolation valves
Oily waste on-shore hook-up	LS	\$6,660	1	\$6,660	
MHP fixed CHT waste piping system	LF	\$55	2456	\$135,601	6" FRTP pipe
CHT waste piping pressure test	HR	\$96	64	\$6,123	16 Hr per section + equipment rental
CHT pipe hangers	EA	\$144	286	\$41,227	Vinylester hanger w SS all-threaded rod
CHT waste sectionalizing valves	EA	\$1,795	32	\$57,424	6" ball valve
CHT waste sectional flex connections	EA	\$554	6	\$3,325	6" braided SS connector, 2' length

Utility Costs for 1300 ft long (4 module) MHP Berthing Facility					
(all costs are installed costs - Navy construction - 2001 \$)					
Item	Units	Unit price	Quantity	Total	Comments
CHT waste hose connectors	EA	\$186	12	\$2,228	Cam-lok fitting
CHT waste outlet valves	EA	\$857	12	\$10,285	4" ball valve
CHT waste MHP to ship hoses (per berth X no. of berths)	EA	\$426	24	\$10,220	50' hose section w cam-lok fittings: (2) sections per utility connection
CHT waste mobile pumping unit	EA	\$21,510	8	\$172,083	
CHT waste line from MHP to on-shore manhole	LF	\$79	800	\$63,216	
CHT waste on-shore hook-up	LS	\$6,660	1	\$6,660	
Motion accommodations provisions MHP to shore	EA	\$5,806	4	\$23,223	6" braided SS connector, 8' long w floating flange + isolation valves
CHT/Oily Waste Manhole	EA	\$7,620	2	\$15,240	
Mechanical Total				\$2,435,962	
Total for 1300 ft MHP Berthing Facility					

MHP Module Towing Costs	\$/day	Mobilization	
7200 BHP - 250,000 lb bollard pull Ocean Tug	\$21,200	\$575,000 Tows large concrete units at 3 kts in open ocean	For reference
A large ocean tug is not needed to tow the MHP modules.			
Estimated costs for a coastal tug (4000 HP)	\$7,800		
Standby and deadhead return for 4 coastal tugs	4	\$93,600 Return without load at 12 kts.	
2 kts = 55 miles per 24 hour day		Tow MHP units at 2 kts in river and coastal waters	
500 mile tow = 9 days	9	\$280,800	
1000 mile tow = 18 days	18		
Total cost 500 mile tow		\$374,400 Baseline cost	
Total cost 1000 mile tow	\$655,200	\$318,240 Low range cost at 85% of baseline	
		\$411,840 High range cost at 110% of baseline	